

## Book Problem Solutions

### Chapter 3 problem solutions

3.4:

Simplex channel = 25kHz => Duplex channel = 50kHz

So 20MHz/50kHz = 400 channels.

If N=4, using omnidirectional antennas => 400/4 = 100 channels per cell site

3.5:

We must compute  $Q^n/i_0$  for each case with  $Q=(3N)^{1/2}$  and  $n=4$ . This simplifies to  $(3N)^2/i_0$ . The 15 db criteria means we need  $(3N)^2/i_0 > 31.62$

- For omnidirectional,  $i_0 = 6$ , so solving for N we get  $N > 4.5 \Rightarrow N = 7$
- For 3 sectored, we check N=4 and N=3 ( $N \geq 7$  will work but we want the smallest N)  
For N=4:  $i_0 = 2$ , so  $(3N)^2/i_0 = 144/2 = 72 > 31.62$ . so N=4 will work with 3 sectors  
For N=3:  $i_0 = 3$ , so  $(3N)^2/i_0 = 81/3 = 27 < 31.62$ . so N=3 will NOT work with 3 sectors.  
So N=4 with 3 sectors is the answer
- For 6 sectors we only need to check N=3 (since  $N \geq 4$  will work)  
For N=3 and  $i_0 = 2$  (for N=3 or 12 or when i-j we must be careful of  $i_0$ )  
So  $(3N)^2/i_0 = 81/2 = 40.5 > 31.62$ . so N=3 WILL work with 6 sectors..... theoretically.....

NOTE: as for which one is the best, you would need to check which provided the highest capacity per basestation. This is tricky. For a large number of channels (e.g. 108 total) you get:

N=7 => 15 ch/bstn => 8.1E per bstn

N=4 with 3 sectors => 27ch/bstn => 9 ch/sector => 3.75E/sector => 11.25E/bstn

N=3 with 6 sectors => 36ch/bstn => 6 ch/sector => 1.9E/sector => 11.4E/bstn

So N=3 wins.... But just barely and (it turns out) not if there are fewer channels (e.g. try 64 ch).

3.8:

As above with  $n=3$  we need  $(3N)^{1.5}/i_0 > 31.62$ :

- $i_0 = 6$ , so  $N > 11.006 \Rightarrow N = 12$
- $i_0 = 2$ , so  $N > 5.29 \Rightarrow N = 7$
- $i_0 = 1$ , so  $N > 3.33 \Rightarrow N = 4$

Now it makes more sense to use 60 degree sectoring (i.e. six sector cells) since we get a better value for N.

3.10:

Duplex channel = 60kHz so 24MHz/60kHz = 400 channels.  $A_u = 0.1 E$ .

- 400/4=100 per cell. Assuming old style AMPS/DAMPS we need 1 cntl channel per cell so that leave 99 tch per cell.
- Perfect scheduling would be 99 circuits in use on each cell. 90% of that means 89.1 circuits in use so we have 99 channels serving 89.1E of users. Now if  $A_u = .1E$  this means we can serve 891 users per cell
- From the chart I gave in class 99 channels gives ~89.1E with GOS = 0.03. or 3% blocking probability (roughly)

- d) With 120 degree sectoring, we get 33 channels per cell/sector on two sectors and 34 on the third for each basestation. So we have 32 TCH and one CNTL per sector for two sectors and 33 TCH one CNTL for the third on each basestation. So from the Erlang B chart: for 32 TCH channels at a 0.03 GOS we get 24.9E or 249 users and for 33 channels at 0.03 GOS we get 25.8E or 258 users. This give a total of 756 users that each basestation can support.
- e)  $50 \times 50 = 2500$  square km so if each basestation covers 5 square km, this give 500 basestations. So in the omnidirectional case we can serve  $500 \times 891 = 445500$  customers
- f)  $500 \times 756 = 378000$  customers.

3.11:

I am interpreting 57 channels as meaning 57 channels per cell/basestation in the omnidirectional case (If all you have is 57 channels for a system, I'd quit now and take up knitting) I will also assume that (like AMPS) control channels are in a separate part of the spectrum and the 57 refers to traffic channels only.  $GOS=0.01$  so in the omnidirectional case each cell can handle 44.22E.  $H=2$ min and  $\lambda=1$ /hr so  $A_u=1/30=0.0333$  E. Thus each cell can handle  $44.22/0.0333=1326.6$  users (on average). With 60 degree sectoring we get 3 sectors with 10 channels and 3 with 9. 10 channels  $\Rightarrow 4.46E \Rightarrow 133.8$  users while 9 channels  $\Rightarrow 3.78E \Rightarrow 113.4$  So the total users declines to 741.6 with sectoring.

3.13:

300 traffic channels (we assume control channels are handled separately) with  $N=4 \Rightarrow 75$  channels cell. 0.01 GOS  $\Rightarrow 60.73E$  per cell.  $A_u=0.04E \Rightarrow 1518.25$  users per cell. For 84 cells  $\Rightarrow 127533$  total users on the system

$N=7 \Rightarrow 43$  channels per cell for 6 cells (one has 42). 0.01 GOS  $\Rightarrow 31.66$  (30.77 for one).

$A_u=0.04 \Rightarrow 791.5$  (769.25)  $\Rightarrow 66219$  users on the system

$N=12 \Rightarrow 25$  channels per cell. 0.01 GOS  $\Rightarrow 16.125$  E per cell.  $A_u=0.04 \Rightarrow 403.125$  users per cell  $\Rightarrow 33862.5$  users on the system.

3.15 is not a good problem.

3.16:

We use  $P/P_0 = (d/d_0)^{-n}$  where  $P_0 = 1$  mW,  $d_0 = 1$  m,  $n=3$ , and  $P=-100$ dBm  $= 10^{-10}$ mw. So we get  $10^{10} = d^3 \Rightarrow d = 10^{3.333} = 2154.4$  m  $= 2.1544$ km. Now the ratio between the distance between cells and the major cell radius  $D/R = Q=(3N)^{1/2}$ . So:  $R = 2.1544 / (3N)^{1/2}$  km so

$N=7 \Rightarrow R = \sim 470$  m

$N=4 \Rightarrow R = \sim 622$ m

## Chapter 4 problem solutions

4.1

Linear version:

$$Pr = Pt \left( \frac{\lambda}{4\pi d} \right)^2 G_t G_r. \lambda = (300\text{m}/\mu\text{s})/900\text{MHz} = 0.333\text{m} \quad d = 1000\text{m}. \quad G_t = G_r = 1$$

$$\text{So: } Pr = 10 \left( \frac{0.333}{4000\pi} \right)^2 = 7.022 \times 10^{-9} \text{ W}$$

Decibel version:

$$Pr = Pt + G_t + G_r - \text{FSL}. \quad Pt = 40 \text{ dBm}, \quad \text{FSL} = 20\log(900) + 20\log(1) + 32.45 = 91.53$$

$$\text{So } Pr = 40 - 91.53 = -51.53 = 7.023 \times 10^{-6} \text{ mw} = 7.023 \times 10^{-9} \text{ W}$$

4.3

The gain of an antenna is given by  $G = A\eta 4\pi/(\lambda^2)$  where  $A\eta$  is the effective aperture (as I mentioned briefly when deriving the FSL equations).  $A$  is the area and  $\eta$  is the efficiency (usually between .4 and .8) For the sake of this problem we can guess that  $\eta = \sim 0.5$

$$f = 60\text{GHz} \text{ so } \lambda = (0.3\text{m/ns})/60\text{GHz} = 0.005\text{m}.$$

$$\text{This gives } G = (0.046 * 0.035) * 0.5 * 4 * \pi / (0.005)^2 = 404.637 = \sim 26 \text{ dB}. \text{ Forget the HPBW.}$$

For the Fraunhofer distance: the largest dimension of the antenna is 0.046m.

$$\text{So } 2D^2/\lambda = 2(0.046)^2/(0.005) = 0.846\text{m} = 84.6 \text{ cm}$$

4.4

$$1\text{W} = 30 \text{ dBm}. \text{ Given the gain is } 26 \text{ db (above), EIRP} = 56\text{dBm}.$$

$$\text{FSL} = 20\log(d_{\text{km}}) + 20\log(60000) + 32.45. \quad \text{RSL} = \text{EIRP} - \text{FSL} + G_r = 82 - \text{FSL}$$

So:

$$d = 1\text{m} = 0.001\text{km}: \text{FSL} = 20\log(0.001) + 20\log(60000) + 32.45 = 68.01 \quad \text{RSL} = 82 - 68 = 14\text{dBm}$$

$$d = 100\text{m} = 0.1\text{km}: \text{FSL} = 20\log(0.1) + 20\log(60000) + 32.45 = 108.01 \quad \text{RSL} = 82 - 108 = -26 \text{ dBm}$$

$$d = 1000\text{m} = 1\text{km}: \text{FSL} = 20\log(1) + 20\log(60000) + 32.45 = 128.01 \quad \text{RSL} = 82 - 128 = -46 \text{ dBm}$$

4.14:

$$50\text{W} = 47 \text{ dBm}. \quad G_t = 0\text{dB}, \quad G_r = 3\text{dB}. \quad f = 1900\text{MHz}. \quad d = 10\text{km}.$$

$$\text{FSL} = 20\log(10) + 20\log(1900) + 32.45 = 118.03\text{dB}.$$

$$\text{a) } Pr = Pt + G_t - \text{FSL} + G_r = 47 + 0 - 118 + 3 = -68\text{dBm}$$

$$\text{d) } \text{FEL} = 40\log(10000) - 20\log(50) - 20\log(1.5) = 130.46 \text{ so}$$

$$Pr = Pt + G_t - \text{FEL} + G_r = 47 - 130.46 + 3 = -80.46 \text{ dBm}$$

4.19:

$P_t=10W=40dBm$ .  $G_t=10dB$ ,  $G_r=3dB$ ,  $L=1dB$ . So  $EIRP = 49dB$  and  $RSL = EIRP - PL + G_r$  (normally I take  $G_r$  to be zero for the usual cellular situation. However in this case, they are assuming a car with a whip antenna, which will give an extra 3dB gain...).

$f=900MHz$  so  $\lambda=.3333$

We will do this backwards: Total distance= 5 km. So:

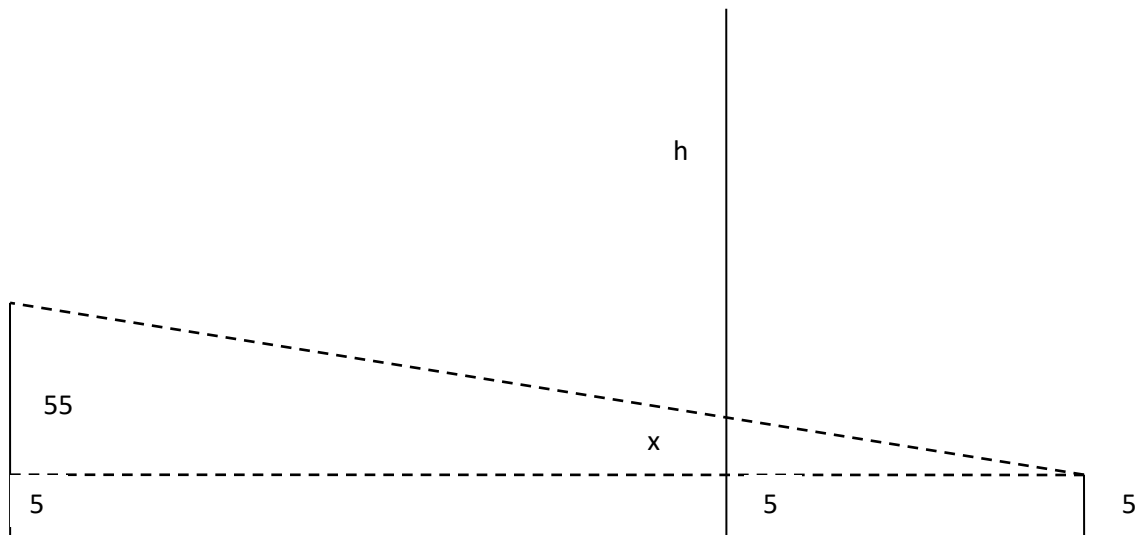
$$FSL = 20\log(900) + 20\log(5) + 32.45 = 105.51 \text{ dB}$$

So,  $RSL$  without diffraction =  $49 - 105.51 + 3 = -53.51dBm$

For diffraction, we do the usual geometry stunt and get

$$400 = 5 + x + h$$

where 5 is the height of the mobile,  $h$  is the height of the obstruction above line of sight, and  $x$  is given by  $55/5 = x/2$ . So  $x = 22m$  and  $h = 373m$  See the drawing below



$$\text{Now } v = h [ 2(5000)/(\lambda(2000)(3000)) ]^{1/2} = 373 ( 1/200 )^{1/2} = 26.375$$

Using 4.61e we get

$$G_d = 20\log(0.225/v) = -41.38 \text{ dB}$$

So  $RSL$  with diffraction =  $-53.51 - 41.38 = -94.89 \text{ dBm}$

4.20: We use the same equations:

a)  $f=50\text{MHz} \Rightarrow \lambda=6\text{m}$  FSL =  $20\log(50) + 20\log(5) + 32.45 = 80.41\text{dB}$

RSL without diffraction =  $49 - 80.41 + 3 = -28.41\text{ dBm}$

$v = 373 [ 2(5000) / ( 6(2000)(3000) ) ]^{1/2} = 6.2167$

$G_d = 20\log(0.225/v) = -28.83\text{ dB}$

RSL with diffraction =  $-28.41 - 28.83 = -57.24\text{ dBm}$

b)  $f=1900\text{MHz} \Rightarrow \lambda=0.15789\text{m}$  FSL =  $20\log(1900) + 20\log(5) + 32.45 = 112\text{ dB}$

RSL without diffraction =  $49 - 112 + 3 = -60\text{ dBm}$

$v = 373 [ 2(5000) / ( (0.15789)(2000)(3000) ) ]^{1/2} = 38.3221$

$G_d = 20\log(0.225/v) = -44.63\text{ dB}$

RSL with diffraction =  $-60 - 44.63 = -104.63\text{ dBm}$

4.23:

This is a challenging (and confusing) exercise in using  $P/P_0 = (d/d_0)^{-n}$  where  $P_0 = 1\mu\text{W}$ ,  $d_0 = 1\text{km}$  and  $d = 2, 5, 10,$  and  $20\text{ km}$ . The value of  $n$  varies with the model:

a) Free space  $\Rightarrow n=2$

b)  $n=3$

c)  $n=4$

d) for the approximate equation for FEL,  $n=4$  as well

e)  $n$  will be the coefficient of the  $\log(d)$  term (divided by 10) =

$[44.9 - 6.55\log(h)]/10 = 4.49 - 6.55\log(40) = 3.44$

P for d=	2km	5km	10km	20km
a) $n=2$	0.25 $\mu\text{W}$	0.04 $\mu\text{W}$	10nW	2.5nW
b) $n=3$	0.125 $\mu\text{W}$	8nW	1nW	0.125nW
c) $n=4$	62.5nW	1.6nW	0.1nW	6.25pW
d) FEL	62.5nW	1.6nW	0.1nW	6.25pW
e) $N=3.44$	92.1nW	3.94nW	0.363nW	33.45pW

## Chapter 5 problem solutions

5.1:

The Doppler shift is given by  $f_d = (v/\lambda)\cos(\theta)$ . The maximum will be when  $\cos = +1$  and the minimum will be at  $\cos = -1$  so we need only compute  $f_m = v/\lambda$  and then add and subtract. We must be careful of the units, however:  $1\text{km/hr} = 0.2778\text{ m/s}$ . Also:  $\lambda = 3 \times 10^8 / 1.95 \times 10^9 = 0.1538\text{m}$  and watch the significant digits:

- $1\text{km/hr} = 0.2778\text{ m/s} \Rightarrow f_m = 1.8056\text{ Hz} \Rightarrow \text{max}f = 1950.000002\text{MHz}$   $\text{min}f = 1949.999998\text{MHz}$
- $5\text{km/hr} = 1.3889\text{ m/s} \Rightarrow f_m = 9.0278\text{ Hz} \Rightarrow \text{max}f = 1950.000009\text{MHz}$   $\text{min}f = 1949.999991\text{MHz}$
- $100\text{km/hr} = 27.78\text{ m/s} \Rightarrow f_m = 180.56\text{ Hz} \Rightarrow \text{max}f = 1950.000181\text{MHz}$   $\text{min}f = 1949.999819\text{MHz}$
- $1000\text{km/hr} = 277.8\text{ m/s} \Rightarrow f_m = 1805.6\text{ Hz} \Rightarrow \text{max}f = 1950.001806\text{MHz}$   $\text{min}f = 1949.998179\text{MHz}$

5.8:

For P5.6a:

We have 4 components so

$$\bar{\tau} = [0(1) + 50(1) + 75(.1) + 100(.01)]/[1+1+.1+.01] = 58.5/2.11 = 27.725\text{ ns}$$

$$\overline{\tau^2} = [0(1) + 50^2(1) + 75^2(.1) + 100^2(.01)]/2.11 = 3162.5/2.11 = 1498.915\text{ ns}^2$$

$$\sigma = (\overline{\tau^2} - (\bar{\tau})^2)^{1/2} = (1498.915 - 768.682)^{1/2} = 27.02\text{ ns}$$

So for 90%  $B_c = 1/(50 \times 27.02) = 7.4 \times 10^{-4}\text{ GHz} = 740\text{KHz}$  (NB:  $t$  in ns  $\Rightarrow f$  in GHz)

For 50%  $B_c = 1/(5 \times 27.02) = 7.4 \times 10^{-3}\text{ GHz} = 7.4\text{ MHz}$

For P5.6b:

We have 3 components:

$$\bar{\tau} = [0(.01) + 5(.1) + 10(1)]/[1 + .1 + .01] = 10.5/1.11 = 9.459\text{ }\mu\text{s}$$

$$\overline{\tau^2} = [0(.01) + 5^2(.1) + 10^2(1)]/1.11 = 102.5/1.11 = 92.3423\text{ }\mu\text{s}^2$$

$$\sigma = (\overline{\tau^2} - (\bar{\tau})^2)^{1/2} = (92.3423 - 89.4814)^{1/2} = 1.691\text{ }\mu\text{s}$$

So for 90%  $B_c = 1/(50 \times 1.691) = .0118\text{ MHz} = 11.8\text{KHz}$

For 50%  $B_c = 1/(5 \times 1.691) = .118\text{ MHz} = 118\text{KHz}$

5.9:

Binary modulated 25kbps signal  $\Rightarrow$  bit duration  $T = 1/25000 = 40\text{ }\mu\text{s}$

To run without an equalizer, we need to be in a flat fading environment, which means we need  $\sigma \ll T = 40\text{ }\mu\text{s}$ . The book uses a rule of thumb which says “ $\ll$ ” is about a factor of 10 so they get a max  $\sigma$  of about  $4\text{ }\mu\text{s}$

For 8PSK modulated at 75kbps we get 3 bits in every symbol. Thus the symbol rate is 25ksps so  $T$  is again  $40\text{ }\mu\text{s}$  so the answer is the same as above.

5.13:

$f = 900\text{MHz}$  so  $\lambda = 1/3 = 0.333\text{ m}$ . We don't know  $v$ , but we can find it if we get the Doppler frequency from the afd. The afd = 1ms for a signal level (by which I assume they mean power level) of 10 dB below the rms level. So  $\rho = -5\text{dB} = .316$

$$\text{afd} = (e^{\rho^2} - 1) / [\rho f_m (2\pi)^{1/2}] = 1\text{ms} = 0.001\text{ s}$$

$$\text{So } f_m = (e^{0.1} - 1) / [\rho (2\pi)^{1/2} (0.001)] = 132.68\text{ Hz}$$

$$\text{So } v = f_m / \lambda = 44.23\text{ m/s}$$

So in 10s the vehicle travels 442.3 m

To find the number of fades we need the level crossing rate:  $N = \rho f_m (2\pi)^{1/2} e^{-\rho^2} = 95.16$  or about 95

5.28:

$$\text{a) } \bar{\tau} = [0(1) + 1(1) + 2(1)] / [1 + 1 + 1] = 2.1/2.1 = 1\ \mu\text{s}$$

$$\bar{\tau}^2 = [0(1) + 1^2(1) + 2^2(1)] / 2.1 = 4.1/2.1 = 1.9524\ \mu\text{s}^2$$

$$\sigma = (\bar{\tau}^2 - (\bar{\tau})^2)^{1/2} = (1.9524 - 1)^{1/2} = 0.9759\ \mu\text{s}$$

b) all components are > 20db below so after 2  $\mu\text{s}$  we get everything so  $\tau_{\text{max } 20\text{dB}} = 2\ \mu\text{s}$

c) So we require  $T > 10\sigma = 9.759\ \mu\text{s} \Rightarrow$  Symbol rate  $< 1/(10\sigma) = 102.47\text{ ksp/s}$

d) We must compute the coherence time so we need the maximum Doppler shift.

$$v = 30\text{km/hr} = 8.333\text{ m/s}, f = 900\text{ MHz} \Rightarrow \lambda = c/f = 1/3\text{ m so } f_m = v/\lambda = 8.333/.3333 =$$

25Hz. Using the conservative value of  $T_c$  we get 7.16 ms. Using the practical value we get 16.92ms. So depending on what "highly correlated" means, you should get one of these values

5.29:

$f = 6\text{GHz} \Rightarrow \lambda = 0.05\text{ m}$ . Since  $v = 80\text{kph} = 22.222\text{ m/s}$ ,  $f_m = v/\lambda = 444.44\text{ Hz}$

a) Zero crossings about the rms value  $\Rightarrow \rho = 1$  so the lcr =  $N = \rho f_m (2\pi)^{1/2} e^{-\rho^2} = 409.839$  per second

So over 5 seconds you get 2049.19

b)  $\text{Afd} = (e^{\rho^2} - 1) / [\rho f_m (2\pi)^{1/2}] = 1.54\text{ ms}$  (NB: so on average the signal spends about 63.2% of its time below the rms level. This is consistent with the Rayleigh fading model)

c) Again, I assume 20 dB is a power level estimation so  $\rho = 0.1$

$$\text{then } \text{afd} = (e^{\rho^2} - 1) / [\rho f_m (2\pi)^{1/2}] = 90.2\ \mu\text{s}$$

5.30:

We look at each scenario:

a) Urban environment  $\Rightarrow$  slow mobiles, e.g.  $v < 30\text{mph} < 50\text{kph} < 14\text{ m/s}$  so  $f_m < 46.33 < 50\text{Hz}$  so even the conservative value of  $T_c$  is 3.58 ms. Data rate = 500kbps  $\Rightarrow T_s = 2\ \mu\text{s}$  so the fading is definitely not fast. However, to pass a 500kbps signal, the channel would need a coherence bandwidth (using the 50% coherence) of 500kHz so  $\sigma < 0.4\ \mu\text{s}$ . This is not likely in an urban fading environment (see , e.g. problem 5.28 or 5.8b above ) Thus this should be frequency selective fading scenario.

b) For a highway environment  $v$  is much larger, so say  $v = 60\text{mph}$  so  $f$  may be 100Hz. Using the practical value give  $T_c = 4.23\text{ ms}$  (conservative gives 1.8ms). Data rate of 5kbps  $\Rightarrow T_s = 0.2\text{ ms}$  so the environment is still pretty slow (i.e. not a fast fading

- environment). However a 5 kHz signal requires only that  $\sigma < 40 \mu\text{s}$ . This is a pretty easy requirement to meet for most channels. Thus this is likely to be a flat fading scenario.
- c) At 10bps,  $T_s = 100\text{ms}$ .  $T_c$  is going to be much less than this (as describe in b and a above) so the environment is clearly fast fading. ( the requirement on  $\sigma$  will be on the order of milliseconds so the environment will also be flat)

Revised 3/12/12